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(71) Applicant: HON

HONDA MOTOR CO LTD

(72) Inventor:

SHIMIZU YASUO

WATANABE KATSUJI YAMAWAKI SHIGERU

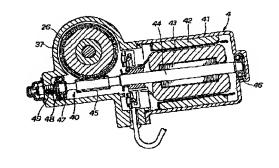
# (54) MOTOR DRIVEN POWER STEERING DEVICE

(57) Abstract:

PROBLEM TO BE SOLVED: To improve a steering feeling by integrally forming the shaft of a motor and the worm shaft of a worm gear mechanism to be an output shaft and supporting both ends of this output shaft so as to be rotated.

SOLUTION: A torque transmitting means 40 for transmitting auxiliary torque generated by a motor 4 to a steering system is composed of a housing 37, a worm 45 and a wheel 26. The output shaft 44 of the motor 4 is a long shaft being extended into the housing 37 and the worm 45 is integrally formed in this shaft. That is, the output shaft 44 is one wherein the shaft of the motor 4 and the worm shaft of the torque transmitting means (worm gear mechanism) 40 are integrally formed. Thus, since no gaps are generated because it not necessary to fit in and connect the worm shaft of the worm gear mechanism 40 to the shaft of the motor 4 and unnecessary play in the rotation of a steering wheel caused by such gaps is eliminated, a steering feeling is improved.

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# **DETAILED DESCRIPTION**

[Detailed Description of the Invention]

[The technical field to which invention belongs] this invention relates to enhancement of electric power-steering equipment. [0002]

[Description of the Prior Art] In order to mitigate the control force of a steering handle and to give the comfortable feeling of steering in recent years, electric power-steering equipment has been used abundantly. This kind of electric power-steering equipment generates the supplementary-with motor torque according to steering torque, transmits this supplementary torque to a steering system through a worm-gearing style and a friction engagement means of communication, and has the technique of JP,60-188064,U "the lock cancel equipment of a motorised type steering system."

[0003] According to drawing [of the official report] 1, - view 3, this technique is an electrical motor 21 (the number quoted what was indicated by the official report.). It is below the same. The warm shaft 27 of a worm-gearing style is fitted in at the nose of cam of an output shaft, a worm gearing 22 is connected with this warm shaft 27 through a freewheel clutch, a worm gear 23 is engaged to this worm gearing 22, and a pinion shaft 24 is connected with this worm gear 23.

[Problem(s) to be Solved by the Invention] However, since it is the configuration which fitted in the warm shaft 27 at the nose of cam of the output shaft of an electrical motor 21, an opening occurs inevitably in fitting of both shafts and excessive play appears in rotation of a steering handle by this opening, a steering feeling becomes bad. Moreover, since the ends of the warm shaft 27 are supported, the distance between bearing is short, and for this reason, the warm shaft 27 seldom bends. There is a possibility that \*\*\*\* may become large since there are few amounts of bending of the warm shaft 27 when a worm gear 23 carries out thermal expansion and presses a worm gearing 22, and a steering feeling may become [frictional resistance] large bad. Furthermore, in order to support the ends of an output shaft, and the ends of the warm shaft 27, four bearing is needed, and the quantity of bearing increases. For this reason, it is not easy for the number of erectors of a motor and a worm-gearing style to be applied, and to raise a productivity, and it seldom aims at a cost cut.

[0005] The purpose of this invention is shown in aiming at a cost cut while it reduces the quantity of the bearing of offering the electric power-steering equipment which improved, \*\* motor, and a worm-gearing style and raises the productivity of a motor and a worm-gearing style.

[0006]

[Means for Solving the Problem] In order to attain the above-mentioned purpose, invention according to claim 1 generates the supplementary-with motor torque according to steering torque, in the electric power-steering equipment which transmits this supplementary torque to a steering system through a worm-gearing style, forms the shaft of the aforementioned motor, and the worm shaft of the aforementioned worm-gearing style in one, and considers as an output shaft, and it is characterized by supporting the both ends of this output shaft possible [ rotation ].

[0007] For this reason, like the conventional technique, on the shaft of a motor, since it is not necessary to carry out the fitting link of the worm shaft of a worm-gearing style, an opening does not occur, but the excessive play of invention according to claim 1 is lost to rotation of the steering handle by this opening, and a steering feeling becomes high. Moreover, since the distance between bearing is long, an output shaft tends to bend rather than the conventional technique. For this reason, since an output shaft bends when a wheel carries out thermal expansion and presses a worm, \*\*\*\* does not become excessive, but frictional resistance can be mitigated, and a steering feeling increases. Furthermore, since the quantity of bearing can be decreased to two pieces, the number of parts decreases, since the number of erectors of a motor and a worm-gearing style becomes fewer, a productivity improves, and it becomes easy to aim at a cost cut. Furthermore, since it is the configuration which supports the output shaft equipped with Rota of a motor, and the worm only by two points of both ends again, the attachment precision of an output shaft is high and \*\*\*\*\*\* also becomes good.

[Embodiments of the Invention] The example of this invention is explained below based on an accompanying drawying. In addition, a drawing shall be seen to the sense of a sign. First, the 1st example is explained based on drawing 1 - view 4.

Drawing 1 is the whole electric power-steering equipment block diagram concerning this invention. the electric power-steering equipment 1 A steering torque detection means 3 to detect the steering torque of the steering system generated by the steering handle 2, The motor 4 which adds supplementary torque to a steering system, and the control unit 5 for controlling a motor 4, It has the friction engagement means of communication 30 and the torque means of communication 40

which transmit the supplementary torque which the aforementioned motor 4 generates to a steering system, and wheels 8 and 8 are \*\*\*\*ed through a pinion 6 and the rack 7.

[0009] <u>Drawing 2</u> is an important section enlarged view of the electric power-steering equipment (the 1st example) concerning this invention, and the upper part fits into the spline 14 of the lower part of the input shaft 11 rotated by the aforementioned steering handle 2, the torsion bar spring 13 which was combined with this input shaft 11 through the pin 12, and was installed below, and this torsion bar spring 13, and it constitutes a main steering system from an output shaft 15 by which the aforementioned pinion 6 was engraved on the lower part. the member to whom angle of torsion generates a torsion bar spring 13 correctly to torque literally -- it is -- relative torsion between an input shaft 11 and the output shaft 15 -- a variation rate is generated

[0010] The steering torque detection means 3 shown in <u>drawing 1</u> consists of a torsion bar spring 13, a slider 23, and a variable-inductance formula sensor 24. namely, the thing which the steering torque detection means 3 spans with the slider 23 of the shape of a cylindrical shape equipped with the inclination slot 21 and the straight slot 22 between the aforementioned input shaft 11 and the output shaft 15 -- it is -- relative torsion -- according to a variation rate, the variation rate of the slider 23 is carried out to shaft orientations The amount of displacement to the shaft orientations of a slider 23 is proportional to torque, and a sensor 24 changes the amount of displacement into an electrical signal.

[0011] Furthermore, the aforementioned friction engagement means of communication 50 fits loosely the metal wheels 26, such as phosphor bronze and cast iron, loosely into the base periphery of an output shaft 15. Friction surface 31a of the concavity of a truncated-cone form which is a cross-section abbreviation taper-like is formed in the input member 31 as which it served with this wheel 26. Moreover, the output member 32 which has friction surface 32a of the heights of a truncated-cone form which is a cross-section abbreviation taper-like possible [a shaft-orientations move] was fitted into the periphery of an output shaft 15, and it constituted from pressing this output member 32 to the aforementioned input member 31 with the compression spring 33 as a press means. The inside of drawing and 35 are housing with which a key, and 36 and 36 contain bearing and 37 contains a worm-gearing style.

[0012] Drawing 3 is a 3-3 line cross section of drawing 2, and shows the cross-section structure of a motor 4 and a torque means of communication 40. A motor 4 consists of a metal output shaft 44 which attached a case 41, the stator 42, Rota 43, and this Rota 43. The aforementioned torque means of communication 40 transmits the supplementary torque which the motor 4 generated to a steering system, and constitutes it from a worm-gearing style which consists of the aforementioned housing 37, and a worm 45 and the wheel 26. In addition, bolt combination of the case 41 of a motor 4 is carried out at housing 37. [0013] By the way, the output shaft 44 of a motor 4 is a long shaft prolonged in housing 37, and forms the worm 45 in this shaft at one. That is, the long output shaft 44 forms the shaft of a motor 4, and the worm shaft of a torque means of communication (worm-gearing style) 40 in one. Thus, on the shaft of a motor 4, since it is not necessary to carry out the fitting link of the worm shaft of the worm-gearing style 40, an opening does not occur, but excessive play is lost to rotation of the steering handle 2 by this opening.

[0014] Moreover, the both ends of an output shaft 44 are made into a thin path, and are supported possible [ rotation ] by two bearing (the 1st bearing 46 and the 2nd bearing 47). That is, an output shaft 44 is supported by the 1st bearing 46 in the back end section, and a point is supported by the 2nd bearing 47. The 2nd bearing 47 fits in possible [ a shaft-orientations move into housing 37 ], and is pressed by the adjusting bolt 49 through flat spring 48 at the Rota 43 side. Therefore, the 1st-2nd bearing 46 and 47 can give a preload according to the press force of an adjusting bolt 49 and the flat spring 48, and it is adjusted so that there may be no end play (backlash \*\*\*\*). Moreover, an output shaft 44 has the thermal expansion of shaft orientations etc. absorbed by the elastic force of flat spring 48. Thus, since the 1st-2nd bearing 46 and the distance between 47 are long, an output shaft 44 tends to bend. For this reason, when a wheel 26 carries out thermal expansion in the orientation of a path and presses a worm 45, the bending rigidity of an output shaft 44 does not become excessive by the parvus's, but \*\*\*\* can mitigate frictional resistance.

[0015] In the electric power-steering equipment 1 which consists of the above configuration, an operation of a friction engagement means of communication 50 is explained based on drawing 4. Drawing 4 is operation explanatory drawing of a friction engagement means of communication (the 1st example) concerning this invention. The supplementary torque of a motor 4 travels to the worm 45 formed in the output shaft 44, and rotates a wheel 26. And a rack 7 is driven through a pinion 6 with the compound torque by which the supplementary torque from a motor 4 was added to the steering torque of a steering system (input-shaft 11 -> torsion-bar-spring 13 -> output shaft 15 shown in drawing 2). That is, T2, then compound torque serve as [torque / steering / of a steering system] "T1+T2" in T1 and the supplementary torque from a motor 4. On the other hand, to the torque more than predetermined, between friction surface 31a and friction surface 32a slips, and excessive torque is not transmitted.

[0016] Next, the 2nd example is explained based on <u>drawing 5 - view 9</u>. In addition, the same sign is attached about the same configuration as the 1st above-mentioned example, and the explanation is omitted. <u>Drawing 5</u> is an important section expanded sectional view of the electric power-steering equipment (the 2nd example) concerning this invention, and the configuration of the 2nd example is characterized by a friction engagement means of communication 50 consisting of a friction engagement formula clutch device. The annular input member 52 is fixed to the inner circumference section of a wheel 26, and, on the other hand, the tubed output member 53 is being fixed to the periphery section of an output shaft 15. The input member 52 fits loosely into the periphery section of the output member 53 through bearing 54. [0017] <u>Drawing 6</u> is a 6-6 line cross section of <u>drawing 5</u>, and shows the configuration which combined a torque means of communication 40 and a friction engagement means of communication 50. The torque means of communication 40 of this

example makes arrangement of a wheel 26 to the center of a worm 45 the 1st example and opposite side which are shown in the above-mentioned  $\underline{\text{view }3}$  . and the center top of a wheel 26 -- and a friction engagement means of communication 50 is arranged on the same field as a wheel 26

[0018] <u>Drawing 7</u> is an expanded sectional view of a friction engagement means of communication (the 2nd example) concerning this invention, and expands and shows the friction engagement means of communication 50 shown in the above-mentioned <u>view 6</u>. The friction engagement means of communication 50 is 6 sets of friction engagement formula clutch devices 51 arranged on the same circle. -- (-- shows a plurality.) below the same \*\*\*\* -- it becomes In addition, in distinguishing each clutch device 51 -- mutually and explaining it, it explains like the clutch devices 51A, 51B, ...., 51F for convenience.

[0019] These clutch device 51 -- consists of taper-like space section 55 -- formed between the input member 52, the output member 53, these inputs / output member 52, and 53, engagement member 56-- by which it was placed between these taper-like space section 55 --, positional-controller member 58-- of this engagement member 56 -- to position, and compression spring 59-- which energizes engagement member 56 -- toward this positional-controller member 58 --. And a friction engagement means of communication 50 is a thing of positional-controller member 58 -- which switches the input member 52 and the output member 53 to engagement and being un-engaged alternatively by engagement member 56 -- in connection with a move.

[0020] If it explains in full detail, between the internal surface of the input member 52 which presents a cylinder cross section, and the three sides of the output member 53 which presents in general a conclusion form cross section (configuration which made circular the three sides of an abbreviation equilateral-triangle cross section), taper [ of a total of three pairs ]-like space section 55 -- will be formed by one pair of right and left for every side, and, as for these taper-like space section 55 --, a hoop-direction edge will be formed in the shape of a taper. Circular cylinder-like engagement member 56 -- is arranged possible [ a move ] at the one hoop-direction edge at each taper-like space section 55 -- of each, and compression spring 59 intervenes between two engagement members 56 which counter mutually, and 56.

[0021] It is the taper-like space section 55 which three positional-controllers member 58 -- intervenes possible [ rotation ] between the internal surface of the input member 52, and the crowning of the output member 53, and each positional-controller member 58 -- adjoins. -- It projects inside and is contacted with engagement member 56 --. Thus, it is arranged on the same circle, estranging three positional-controllers member 58 -- at equal intervals mutually. [0022] thus, the constituted friction engagement means of communication 50 -- the -- 1 and the 3rd-5th clutch devices 51A, 51C, and 51E -- the orientation (the orientation of a counterclockwise rotation of this drawing) of arrow head X of the input member 52 -- being engaged -- the -- 2 and the 4th-6th clutch devices 51B, 51D, and 51F are engaged in arrow head X and

the opposite orientation

[0023] <u>Drawing 8</u> is an important section decomposition perspective diagram of a friction engagement means of communication (the 2nd example) concerning this invention, the input shaft 11 is fixing the annular positional-controller section 57 to a soffit periphery, and this positional-controller section 57 equips the lower part with aforementioned three positional-controllers member 58 --.

[0024] Next, an operation of the friction engagement means of communication of the above-mentioned configuration is explained based on the <u>drawing 7</u> and the <u>drawing 9</u>. <u>Drawing 9</u> is an operation view of a friction engagement means of communication (the 2nd example) at this invention. When the steering handle 2 is not steered, as shown in <u>drawing 7</u>, each clutch device 51 — of all is canceled.

[0025] The phase between the output members 53 hardly changes [ the steering torque of a steering handle 2 ] with each positional-controller member 58 — of an input shaft 11 a parvus case. In this case, although each positional-controller member 58 — moves in the orientation of a counterclockwise rotation of this drawing a little, each clutch device 51 — does not have \*\* et al. in being engaged. For this reason, the output member 53 does not receive the supplementary torque from a motor 4, but the control force which acts on an input shaft 11 is transmitted to the output member 53 through a torsion bar spring 13. [0026] Next, when the steering torque of a steering handle 2 is large, the phase between the output members 53 changes a lot with each positional-controller member 58 — of an input shaft 11. In this case, as shown in drawing 9, each positional-controller member 58 — moves in the orientation of arrow head X greatly. the [ for this reason, ] — 1 and the 3rd-5th clutch devices 51A, 51C, and 51E will be in the engagement status (Engagement member 56 — is pushed on compression spring 59 —, moves, and is engaged in the input member 52 and the output member 53 with frictional force). [0027] a motor 4 rotates — the input member 52 — the orientation of arrow head X — rotating — the supplementary torque from a motor 4 — the — it is transmitted to the output member 53 (steering system) through 1 and the 3rd-5th clutch devices 51A, 51C, and 51E Therefore, the output member 53 is the compound torque by which the supplementary torque from a motor 4 was added to the steering torque of the steering system (input-shaft 11 — torsion-bar-spring 13 — output shaft 15) in drawing 5, and is driven in the orientation of arrow head X.

[0028] On the other hand, if a steering handle 2 is steered to an opposite direction in the status that transmission of the supplementary torque by the motor 4 is continuing, it will turn around each positional-controller member 58 -- in the input member 52 and the opposite orientation (arrow head X and the opposite orientation). the [for this reason, ] -- 1 and the 3rd-5th clutch devices 51A, 51C, and 51E will be in the cancel status (Engagement member 56 -- is pushed on positional-controller member 58 --, moves, and cancels the friction engagement between the input member 52 and the output member 53.)

[0029] In addition, 3 sets of clutch devices 51B, 51D, and 51F engaged in the orientation of a reverse rotation carry out 3 sets

of clutch devices 51A, 51C, and 51E and a reverse action besides the above, and when a steering handle 2 is steered in the opposite orientation, they are switched to engagement and being un-engaged.

[0030] In addition, although the 1st-2nd above-mentioned example explained the wheel 26 as metal, the effect same also as products made from a resin, such as nylon, as each example can be done so for this.

[Effect of the Invention] this invention demonstrates the following effect by the above-mentioned configuration. The shaft of the motor for invention according to claim 1 generating the supplementary torque according to steering torque, By having formed the worm shaft of the worm-gearing style for transmitting supplementary torque to a steering system in one, having used it as the output shaft, and having supported it possible [ rotation of the both ends of this output shaft ] Like the conventional technique, on the shaft of a motor, since it is not necessary to carry out the fitting link of the worm shaft of a worm-gearing style, an opening does not occur, but excessive play is lost to rotation of the steering handle by this opening, and a steering feeling becomes high.

[0032] Moreover, since the distance between bearing is long, an output shaft tends to bend rather than the conventional technique. For this reason, since an output shaft bends when a wheel carries out thermal expansion and presses a worm, \*\*\*\* does not become excessive, but frictional resistance can be mitigated, and a steering feeling increases. Furthermore, since the quantity of bearing can be decreased to two pieces, the number of parts decreases, since the number of erectors of a motor and a worm-gearing style becomes fewer, a productivity improves, and a cost cut can be aimed at. Furthermore, since it is the configuration which supports the output shaft equipped with Rota of a motor, and the worm only by two points of both ends again, the attachment precision of an output shaft is high and \*\*\*\*\*\* is also good.

[Translation done.]

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### **MEANS**

[Means for Solving the Problem] In order to attain the above-mentioned purpose, invention according to claim 1 generates the supplementary-with motor torque according to steering torque, in the electric power-steering equipment which transmits this supplementary torque to a steering system through a worm-gearing style, forms the shaft of the aforementioned motor, and the worm shaft of the aforementioned worm-gearing style in one, and considers as an output shaft, and it is characterized by supporting the both ends of this output shaft possible [ rotation ].

[0007] For this reason, like the conventional technique, on the shaft of a motor, since it is not necessary to carry out the fitting link of the worm shaft of a worm-gearing style, an opening does not occur, but the excessive play of invention according to claim 1 is lost to rotation of the steering handle by this opening, and a steering feeling becomes high. Moreover, since the distance between bearing is long, an output shaft tends to bend rather than the conventional technique. For this reason, since an output shaft bends when a wheel carries out thermal expansion and presses a worm, \*\*\*\* does not become excessive, but frictional resistance can be mitigated, and a steering feeling increases. Furthermore, since the quantity of bearing can be decreased to two pieces, the number of parts decreases, since the number of erectors of a motor and a worm-gearing style becomes fewer, a productivity improves, and it becomes easy to aim at a cost cut. Furthermore, since it is the configuration which supports the output shaft equipped with Rota of a motor, and the worm only by two points of both ends again, the attachment precision of an output shaft is high and \*\*\*\*\*\* also becomes good.

[Embodiments of the Invention] The example of this invention is explained below based on an accompanying drawying. In addition, a drawing shall be seen to the sense of a sign. First, the 1st example is explained based on drawing 1 - view 4.

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[0009] Drawing 2 is the electric power-steering equipment concerning this invention.

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### PRIOR ART

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[0003] According to drawing [of the official report ] 1, - view 3, this technique is an electrical motor 21 (the number quoted what was indicated by the official report.). It is below the same. The warm shaft 27 of a worm-gearing style is fitted in at the nose of cam of an output shaft, a worm gearing 22 is connected with this warm shaft 27 through a freewheel clutch, a worm gear 23 is engaged to this worm gearing 22, and a pinion shaft 24 is connected with this worm gear 23.

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(71) 出顧人 000005326

本田技研工業株式会社

東京都港区南青山二丁目1番1号

(72)発明者 情水 康夫

埼玉県和光市中央1丁目4番1号 株式会

社本田技術研究所内

(72) 発明者 渡辺 勝治

埼玉県和光市中央1丁目4番1号 株式会

社本田技術研究所内

(72)発明者 山脇 茂

埼玉県和光市中央1丁目4番1号 株式会

社本田技術研究所内

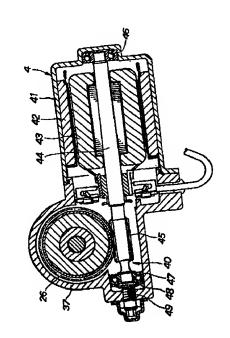
(74)代理人 弁理士 下田 容一郎

# (54) 【発明の名称】 電動パワーステアリング装置

# (57) 【要約】

【解決手段】 電動機4で操舵トルクに応じた補助トル クを発生し、この補助トルクをウォームギヤ機構40を 介してステアリング系に伝達する電動パワーステアリン グ装置において、電動機の軸とウォームギヤ機構のウォ ーム軸とを一体に形成して出力軸44とし、この出力軸 の両端部を回転可能に支持したことを特徴とする電動パ ワーステアリング装置。

【効果】 従来技術のように電動機の軸にウォームギヤ 機構のウォーム軸を嵌合連結する必要がないので隙間が 発生せず、この隙間によるステアリングハンドルの回転 に余分な遊びがなくなり、操舵フィーリングが高くな る。



# 【特許請求の範囲】

【請求項1】 電動機で操舵トルクに応じた補助トルクを発生し、この補助トルクをウォームギヤ機構を介してステアリング系に伝達する電動パワーステアリング装置において、前記電動機の軸と前記ウォームギヤ機構のウォーム軸とを一体に形成して出力軸とし、この出力軸の両端部を回転可能に支持したことを特徴とする電動パワーステアリング装置。

# 【発明の詳細な説明】

[0001]

【発明の属する技術分野】本発明は電動パワーステアリング装置の改良に関する。

# [0002]

【従来の技術】近年、ステアリングハンドルの操舵力を 軽減して快適な操舵感を与えるために、電動パワーステ アリング装置が多用されてきた。この種の電動パワース テアリング装置は、電動機で操舵トルクに応じた補助ト ルクを発生し、この補助トルクをウォームギヤ機構及び 摩擦係合伝達手段を介してステアリング系に伝達するも のであって、例えば実開昭60-188064号「モー タ駆動型ステアリング装置のロック解除装置」の技術が ある。

【0003】この技術は、その公報の図1~図3によれば、電動モータ21(番号は公報に記載されたものを引用した。以下同じ。)の出力軸の先端にウォームギヤ機構のウォームシャフト27を嵌合し、このウォームシャフト27にフリーホイールクラッチを介してウォームギヤ22を連結し、このウォームギヤ22にウォームホイール23を噛み合わせ、このウォームホイール23にピニオンシャフト24を連結したものである。

# [0004]

【発明が解決しようとする課題】しかし、電動モータ2 1の出力軸の先端にウォームシャフト27を嵌合した構 成であり、両軸同士の嵌合には必然的に隙間が発生し、 この隙間によってステアリングハンドルの回転に余分な 遊びがでるので、操舵フィーリングは悪くなる。また、 ウォームシャフト27の両端を支持するので軸受間距離 が短く、このため、ウォームシャフト27は撓みにく い。ウォームホイール23が熱膨張してウォームギヤ2 2を押圧した際に、ウォームシャフト27の撓み量が少 40 る。 ないので歯圧が大きくなり、摩擦抵抗が大きく操舵フィ ーリングが悪くなる恐れがある。更に、出力軸の両端と ウォームシャフト27の両端とを支持するために4個の 軸受を必要とし、軸受の数量が多くなる。このため、電 動機とウォームギヤ機構の組立工数がかかり生産性を高 めることが容易でなく、また、コストダウンを図りにく V١

【○○○5】本発明の目的は、①操舵フィーリングの向

て、電動機とウォームギヤ機構の生産性を高めるととも に、コストダウンを図ることにある。

[0006]

【課題を解決するための手段】上記目的を達成するために、請求項1記載の発明は、電動機で操舵トルクに応じた補助トルクを発生し、この補助トルクをウォームギヤ機構を介してステアリング系に伝達する電動パワーステアリング装置において、前記電動機の軸と前記ウォームギヤ機構のウォーム軸とを一体に形成して出力軸とし、この出力軸の両端部を回転可能に支持したことを特徴とする。

【0007】このため、請求項1記載の発明は、従来技術のように電動機の軸にウォームギヤ機構のウォーム軸を嵌合連結する必要がないので隙間が発生せず、この隙間によるステアリングハンドルの回転に余分な遊びがなくなり、操舵フィーリングが高くなる。また、出力軸は軸受間距離が長いので従来技術よりも撓み易い。このため、ホイールが熱膨張してウォームを押圧した際に出力軸が撓むので、歯圧が過大にならず摩擦抵抗を軽減でき、操舵フィーリングが高まる。更に、軸受の数量を2個に減少できるので部品数が少なくなり、電動機とウォームギヤ機構の組立工数が減るので生産性が向上し、また、コストダウンを図り易くなる。更にまた、電動機のロータとウォームとを備えた出力軸を両端部の2点だけで支持する構成なので、出力軸の組付け精度が高く、組付性も良くなる。

[0008]

【発明の実施の形態】本発明の実施例を添付図面に基づいて以下に説明する。なお、図面は符号の向きに見るものとする。先ず、図1~図4に基づき第1実施例を説明する。図1は本発明に係る電動パワーステアリング装置1は、ステアリングハンドル2で発生されたステアリング系の操舵トルクを検出する操舵トルク検出手段3と、ステアリング系に補助トルクを付加する電動機4と、電動機4を制御するための制御装置5と、前記電動機4の発生する補助トルクをステアリング系に伝達する摩擦係合伝達手段30及びトルク伝達手段40とを有し、ピニオン6、ラック7を介して車輪8、8を転舵するものである。

【0009】図2は本発明に係る電動パワーステアリング装置(第1実施例)の要部拡大図であり、前記ステアリングハンドル2で回動される入力軸11と、この入力軸11にピン12を介して結合され下方へ延設されたトーションバー13と、このトーションバー13の下部のスプライン14に上部が嵌合され、下部に前記ピニオン6が刻設された出力軸15とで主たるステアリング系を構成したものである。トーションバー13は文字通りトルクに対して正確にわけれ角が発生するメンバーであっ

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を発生する。

【0010】図1に示す操舵トルク検出手段3は、トーションバー13、スライダ23及び可変インダクタンス式センサ24で構成する。すなわち、操舵トルク検出手段3は、傾斜溝21とストレート溝22とを備えた円筒形状のスライダ23を、前記入力軸11と出力軸15との間に掛け渡すことで、相対ねじり変位に応じてスライダ23を軸方向へ変位させるものである。スライダ23の軸方向への変位量はトルクに比例し、センサ24は変位量を電気信号に変換する。

【0011】更に、前記摩擦係合伝達手段50は、出力軸15の基部外周にリン青銅や鋳鉄などの金属製ホイール26を遊帐し、このホイール26と兼ねた入力部材31に断面略テーパー状である円錐台形の凹部の摩擦面31aを形成し、また、出力軸15の外周に軸方向移動可能に断面略テーパー状である円錐台形の凸部の摩擦面32aを有する出力部材32を検合し、この出力部材32を押圧手段としての圧縮ばね33で前記入力部材31に押圧することで構成した。図中、35はキー、36,36は軸受、37はウォームギヤ機構を収納するハウジングである。

【0012】図3は図2の3-3線断面図であり、電動機4とトルク伝達手段40の断面構造を示す。電動機4はケース41と、ステータ42と、ロータ43と、このロータ43を取付けた金属製の出力軸44とからなる。前記トルク伝達手段40は、電動機4の発生した補助トルクをステアリング系へ伝達するものであり、前記ハウジング37と、ウォーム45とホイール26とからなるウォームギヤ機構で構成する。なお、電動機4のケース41はハウジング37にボルト結合されている。

【0013】ところで、電動機4の出力軸44はハウジング37内に延びる長い軸であり、この軸にウォーム45を一体に形成している。すなわち、長い出力軸44は電動機4の軸とトルク伝達手段(ウォームギヤ機構)40のウォーム軸とを一体に形成したものである。このように、電動機4の軸にウォームギヤ機構40のウォーム軸を嵌合連結する必要がないので隙間が発生せず、この隙間によるステアリングハンドル2の回転に余分な遊びがなくなる。

【0014】また、出力軸44の両端部は細い径とされ、且つ2個の軸受(第1軸受46と第2軸受47)で回転可能に支持されている。すなわち、出力軸44は後端部を第1軸受46で支持され、先端部を第2軸受47で支持される。第2軸受47はハウジング37内に軸方向移動可能に嵌合され、板ばね48を介して調整ボルト49でロータ43側に押圧されている。従って第1・第2軸受46,47は、調整ボルト49と板ばね48の押圧力により予荷重を与えられて、軸方向の遊びがないよ

このように、出力軸44は第1・第2軸受46,47間 距離が長いので撓み易い。このため、ホイール26が径 方向に熱膨張してウォーム45を押圧した際に出力軸4 4の曲げ剛性が小さいので、歯圧が過大にならず摩擦抵 抗を軽減できる。

【0015】以上の構成からなる電動パワーステアリング装置1において、摩擦係合伝達手段50の作用を図4に基づき説明する。図4は本発明に係る摩擦係合伝達手段(第1実施例)の作用説明図である。電動機4の補助トルクは、出力軸44に形成されたウォーム45に伝わり、ホイール26を回動する。そして、ステアリング系(図2に示す入力軸11→トーションバー13→出力軸15)の操舵トルクに、電動機4からの補助トルクが付加されたところの複合トルクでピニオン6を介してラック7を駆動する。すなわち、ステアリング系の操舵トルクをT1、電動機4からの補助トルクをT2とすれば、複合トルクは「T1+T2」となる。一方、所定以上のトルクに対しては、摩擦面31aと摩擦面32aとの間がスリップし、過大トルクを伝達しない。

【0016】次に、図5~図9に基づき第2実施例を説明する。なお、上記第1実施例と同じ構成については同一符号を付し、その説明を省略する。図5は本発明に係る電動パワーステアリング装置(第2実施例)の要部拡大断面図であり、第2実施例の構成は摩擦係合伝達手段50が摩擦係合式クラッチ機構からなることを特徴とする。ホイール26の内周部に環状の入力部材52が固定され、一方、出力軸15の外周部に筒状の出力部材53が固定されている。出力部材53の外周部には軸受54を介して入力部材52が遊嵌される。

【0017】図6は図5の6-6線断面図であり、トルク伝達手段40と摩擦係合伝達手段50とを組合わせた構成を示す。この実施例のトルク伝達手段40は、ウォーム45の中心に対するホイール26の配置を、上記図3に示す第1実施例と反対側としている。そして、ホイール26の中心上に且つホイール26と同一面上に摩擦係合伝達手段50が配置される。

【0018】図7は本発明に係る摩擦係合伝達手段(第2実施例)の拡大断面図であり、上記図6に示す摩擦係合伝達手段50を拡大して示す。摩擦係合伝達手段5040は同一円上に配置された6組の摩擦係合式クラッチ機構51…(…は複数を示す。以下同じ。)からなる。なお、各クラッチ機構51…を互いに区別して説明する場合には、便宜的にクラッチ機構51A,51B,……,51Fのように説明する。

【0019】これらのクラッチ機構51…は、入力部材52と、出力部材53と、これら入力・出力部材52、53間で形成したテーバ状空間部55…と、このテーパ状空間部55…に介在した係合部材56…と、この係合部は56…のが概違めをかまが機制網路が材58…と、この係合

る圧縮ばね59…とからなる。そして、摩擦係合伝達手段50は位置制御部材58…の移動にともなって、係合部材56…で入力部材52と出力部材53とを係合・非係合に選択的に切換えるものである。

【0020】詳述すると、円筒断面を呈する入力部材52の内壁面と、概ねおむすび形断面(略正三角形断面の3つの辺を円弧状とした形状)を呈する出力部材53の3つの辺との間で、各辺毎に左右1対で計3対のテーパ状空間部55…が形成され、これらのテーパ状空間部55…は周方向端部がテーパ状に形成される。各テーパ状 10空間部55…には円柱状の係合部材56…が周方向端部に1つずつ移動可能に配置され、互いに対向する2つの係合部材56,56間に圧縮ばね59が介在される。

【0021】入力部材52の内壁面と出力部材53の頂部との間に、3つの位置制御部材58…が回動可能に介在され、各位置制御部材58…は隣接するテーパ状空間部55…内に突出して係合部材56…と当接される。このように、3つの位置制御部材58…は、互いに等間隔で離間しつつ同一円上に配置される。

【0022】このように構成された摩擦係合伝達手段50は、第1・第3・第5クラッチ機構51A,51C,51Eが入力部材52の矢印X方向(この図の反時計回り方向)に係合し、第2・第4・第6クラッチ機構51B,51D,51Fが矢印Xと反対方向に係合する。

【0023】図8は本発明に係る摩擦係合伝達手段(第2実施例)の要部分解斜視図であり、入力軸11は下端外周に環状の位置制御部57を固定しており、この位置制御部57は下部に前記3つの位置制御部材58…を備えている。

【0024】次に上記構成の摩擦係合伝達手段の作用を 図7及び図9に基づき説明する。図9は本発明に摩擦係 合伝達手段(第2実施例)の作用図である。ステアリン グハンドル2が操舵されていない場合、図7に示すよう に各クラッチ機構51…は全て解除されている。

【0025】ステアリングハンドル2の操舵トルクが小さい場合、入力軸11の各位置制御部材58…と出力部材53との間の位相がほとんど変化しない。この場合には、各位置制御部材58…がこの図の反時計回り方向に若干移動するものの、各クラッチ機構51…が係合するには致らない。このため、出力部材53は電動機4から40の補助トルクを受けず、入力軸11に作用する操舵力はトーションバー13を介して出力部材53へ伝達される。

【0026】次に、ステアリングハンドル2の操舵トルクが大きい場合、入力軸11の各位置制御部材58…と出力部材53との間の位相が大きく変化する。この場合には図9に示すように、各位置制御部材58…が矢印X方向に大きく移動する。このため、第1・第3・第5ク

摩擦力にて入力部材52と出力部材53とを係合する)。

【0027】電動機4が回転することで入力部材52が 矢印X方向に回転し、電動機4からの補助トルクは、第 1・第3・第5クラッチ機構51A,51C,51Eを 介して出力部材53(ステアリング系)に伝達される。 従って、出力部材53は図5におけるステアリング系

(入力軸 $11 \rightarrow \text{h--} \rightarrow$ 

【0028】一方、電動機4による補助トルクの伝達が継続している状態で、ステアリングハンドル2を逆方向に操舵すると、各位置制御部材58…は入力部材52と反対方向(矢印Xと反対方向)に回る。このため、第1・第3・第5クラッチ機構51A,51C,51Eは解除状態になる。(係合部材56…が位置制御部材58…に押されて移動し、入力部材52と出力部材53との間の摩擦係合を解除する。)

【0029】なお、逆回転方向に係合する3組のクラッチ機構51B,51D,51Fは、上記他の3組のクラッチ機構51A,51C,51Eと逆作動をするものであり、ステアリングハンドル2を反対方向に操舵した場合に係合・非係合に切換えられる。

【0030】なお、上記第1・第2実施例ではホイール26を金属製として説明したが、これをナイロン等の樹脂製としても、各実施例と同様の効果を奏することができる。

[0031]

【発明の効果】本発明は上記構成により次の効果を発揮する。請求項1記載の発明は、操舵トルクに応じた補助トルクを発生するための電動機の軸と、補助トルクをステアリング系に伝達するためのウォームギヤ機構のウォーム軸とを、一体に形成して出力軸とし、この出力軸の両端部を回転可能に支持したことにより、従来技術のように電動機の軸にウォームギヤ機構のウォーム軸を嵌合連結する必要がないので隙間が発生せず、この隙間によるステアリングハンドルの回転に余分な遊びがなくなり、操舵フィーリングが高くなる。

【0032】また、出力軸は軸受間距離が長いので従来技術よりも撓み易い。このため、ホイールが熱膨張してウォームを押圧した際に出力軸が撓むので、歯圧が過大にならず摩擦抵抗を軽減でき、操舵フィーリングが高まる。更に、軸受の数量を2個に減少できるので部品数が少なくなり、電動機とウォームギヤ機構の組立工数が減るので生産性が向上し、また、コストダウンを図れる。更にまた、電動機のロータとウォームとを備えた出力軸を両端部の2点だけで支持する構成なので、出力軸の組付け精度が高く、組付性も良い。

「図面の機能が総明」

# 体構成図

【図2】本発明に係る電動パワーステアリング装置 (第 1 実施例) の要部拡大図

【図3】図2の3-3線断面図

【図4】本発明に係る摩擦係合伝達手段(第1実施例) の作用説明図

【図5】本発明に係る電動パワーステアリング装置(第 2 実施例) の要部拡大断面図

【図6】図5の6-6線断面図

【図7】本発明に係る摩擦係合伝達手段(第2実施例) の拡大断面図

【図8】本発明に係る摩擦係合伝達手段(第2実施例)

の要部分解斜視図

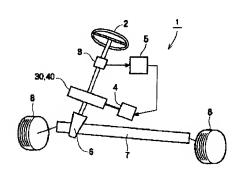
【図9】本発明に摩擦係合伝達手段(第2実施例)の作 用図

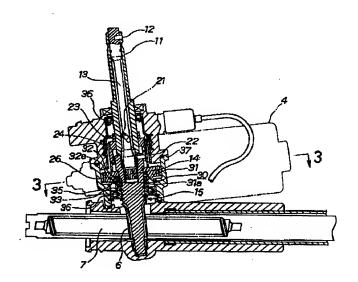
【符号の説明】

1…電動パワーステアリング装置、2…ステアリングハ ンドル、4…電動機、6…ピニオン、7…ラック、11 …入力軸、13…トーションバー、15…出力軸、26 **…ホイール、30…摩擦係合伝達手段、37…ハウジン** グ、40…トルク伝達手段(ウォームギヤ機構)、44 10 …出力軸、45…ウォーム、46…軸受、50…摩擦係 合伝達手段。



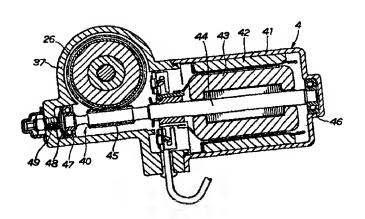




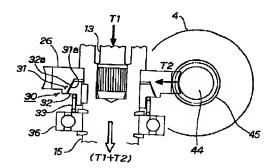


【図2】

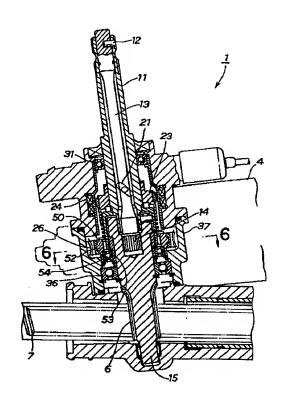
【図3】



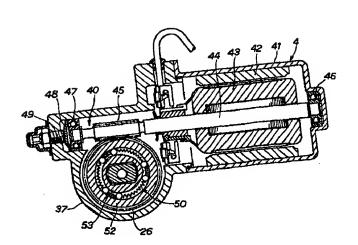
【図4】



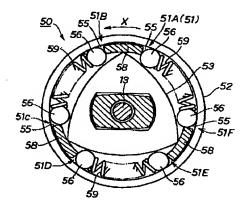
[図5]



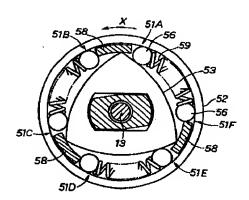
【図6】



【図7】



【図9】



【図8】

